

Fresnel Eqs for reflection: in theory simple
just apply BC for each polarization

BC

$$\begin{matrix} ① \\ \leftarrow n \\ | \\ ② \end{matrix}$$

$$\nabla \cdot \mathbf{B} = 0 \rightarrow B_{1n} = B_{2n}$$

$$\nabla \times \mathbf{E} = -\partial_t \mathbf{B} \rightarrow E_{1t} = E_{2t}$$

$$\begin{aligned} \nabla \cdot \mathbf{D} &= \rho \\ \nabla \cdot \mathbf{J} &= -\partial_t \rho \end{aligned} \rightarrow \left(\epsilon_1 + i \frac{g_1}{\omega} \right) E_{1n}$$

$$\left(\epsilon_2 + i \frac{g_2}{\omega} \right) E_{2n}$$

$$\nabla \times \mathbf{H} = \mathbf{J} + \partial_t \mathbf{D} \rightarrow H_{1t} = H_{2t}$$

Complex g unless $g \rightarrow \infty$ in which case

$$i + \frac{1}{c} J = \frac{N}{m} E \quad E, H \rightarrow 0$$

$$\hookrightarrow g = \frac{N \delta^2 c}{1 - i \omega c} \quad \text{define } \omega_p^2 = \frac{Ng^2}{mc^2}$$

$$0 = (\nabla^2 - \epsilon_R \partial_t^2 - g_R \partial_t) E \quad e^{i(\hat{k}z - \omega t)}$$

$$\epsilon_R + i \frac{g_R}{\omega} = \frac{\hat{k}^2}{\omega^2} = \frac{\hat{n}^2}{c^2} \quad \frac{1}{k_1} = \delta = \text{skin depth}$$

$$\omega \ll \frac{1}{c} \quad g = \frac{N \delta^2 c}{m} \quad \hat{k} = \sqrt{i} \sqrt{g \omega} \quad s = \sqrt{\frac{z}{g \omega}}$$

$$\omega \gg \frac{1}{c} \quad g = \frac{N \delta^2 / m}{-i \omega} \quad r_i = r_o (1 + i)$$

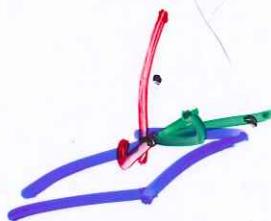
$$n^2 = 1 - \frac{\omega_p^2}{\omega^2}$$



$$F = PA$$



Pressure



Viscosity

S

$$T = \begin{pmatrix} P & G^1 \\ G^2 & P \end{pmatrix}$$

$\rightarrow T \cdot n$
Stress T_{use}

F/A Area

$$\nabla \cdot E = P$$

$\frac{1}{T}$

$$\cdot \square = T_{\mu\nu}$$



$$S T \cdot n dA = \underline{\underline{F}}$$

monomer
Volume

f Ligt

$$P = \frac{E}{C}$$

The Lorentz force per unit volume \mathbf{f} is

$$\mathbf{f} = \rho\mathbf{E} + \mathbf{J} \times \mathbf{B} \quad (8-94)$$

We begin by eliminating the sources ρ and \mathbf{J} , using Maxwell I and Maxwell IV in empty space, giving

$$\mathbf{f} = \varepsilon_0\mathbf{E}\nabla \cdot \mathbf{E} + \frac{1}{\mu_0}(\nabla \times \mathbf{B}) \times \mathbf{B} - \varepsilon_0 \frac{\partial \mathbf{E}}{\partial t} \times \mathbf{B} \quad (8-95)$$

Using the relation

$$\frac{\partial}{\partial t}(\mathbf{E} \times \mathbf{B}) = \frac{\partial \mathbf{E}}{\partial t} \times \mathbf{B} + \mathbf{E} \times \frac{\partial \mathbf{B}}{\partial t} = \frac{\partial \mathbf{E}}{\partial t} \times \mathbf{B} - \mathbf{E} \times (\nabla \times \mathbf{E}) \quad (8-96)$$

we can rewrite Equation (8-95) as

$$\mathbf{f} = \varepsilon_0[\mathbf{E}\nabla \cdot \mathbf{E} + (\nabla \times \mathbf{E}) \times \mathbf{E}] + \frac{1}{\mu_0}[\mathbf{B}\nabla \cdot \mathbf{B} + (\nabla \times \mathbf{B}) \times \mathbf{B}] \quad (8-97)$$

$$-\varepsilon_0 \frac{\partial}{\partial t}(\mathbf{E} \times \mathbf{B})$$

where $\mathbf{B}\nabla \cdot \mathbf{B}/\mu_0 = 0$ is added for reasons of symmetry.

The identity

$$[(\nabla \times \mathbf{E}) \times \mathbf{E}]_i = E_j \left(\frac{\partial E_i}{\partial x_j} - \frac{\partial E_j}{\partial x_i} \right) \quad (8-98)$$

follows directly from expansion in Cartesian coordinates. Here and in the rest of this section a sum is understood over the repeated index j . With this identity and a similar one involving \mathbf{B} , Equation (8-97) becomes

$$\begin{aligned} f_i &= \varepsilon_0 \left(E_i \frac{\partial E_j}{\partial x_j} + E_j \frac{\partial E_i}{\partial x_j} - E_j \frac{\partial E_j}{\partial x_i} \right) + \frac{1}{\mu_0} \left(B_j \frac{\partial B_i}{\partial x_j} + B_i \frac{\partial B_j}{\partial x_j} \right. \\ &\quad \left. - B_j \frac{\partial B_i}{\partial x_i} \right) - \varepsilon_0 \frac{\partial}{\partial t}(\mathbf{E} \times \mathbf{B})_i \end{aligned} \quad (8-99a)$$

This relation can be reexpressed as

$$\begin{aligned} f_i &= \varepsilon_0 \frac{\partial}{\partial x_j} \left(E_i E_j - \frac{1}{2} \delta_{ij} E^2 \right) + \frac{1}{\mu_0} \frac{\partial}{\partial x_j} \left(B_i B_j - \frac{1}{2} \delta_{ij} B^2 \right) \\ &\quad - \varepsilon_0 \frac{\partial}{\partial t}(\mathbf{E} \times \mathbf{B})_i \end{aligned} \quad (8-99b)$$

where δ_{ij} is the Kronecker delta ($\delta_{ij} = 1$ for $i = j$ and $\delta_{ij} = 0$ for $i \neq j$).

The Maxwell stress tensor is defined as follows:

Maxwell Stress Tensor	$T_{ij} \equiv \varepsilon_0 E_i E_j + \frac{1}{\mu_0} B_i B_j - \frac{1}{2} \delta_{ij} \left(\varepsilon_0 E^2 + \frac{1}{\mu_0} B^2 \right)$
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The field momentum volume density is defined as follows:

Field Momentum Density	$\mathbf{P}_{\text{field}} = \varepsilon_0 \mathbf{E} \times \mathbf{B}$
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$$T_{ij} \equiv \varepsilon_0 E_i E_j + \frac{1}{\mu_0} B_i B_j - \frac{1}{2} \delta_{ij} \left(\varepsilon_0 E^2 + \frac{1}{\mu_0} B^2 \right) \quad (8-100)$$

Momentum Conservation	$\frac{d}{dt}(\mathbf{P}_{\text{charges}} + \mathbf{P}_{\text{field}})_i = \oint T_{ij} dS_j$
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In terms of these quantities Equation (8-99b) is

$$f_i = \frac{\partial T_{ij}}{\partial x_j} - \frac{\partial(\rho_{\text{field}})}{\partial t} \quad (8-102)$$

When Equation (8-102) is integrated over a finite volume, the momentum conservation law is obtained. With only electromagnetic forces acting, the momentum change of the charges is related by Newton's second law to the volume force by

$$\frac{d(\mathbf{P}_{\text{charges}})_i}{dt} = \mathbf{F}_i = \int \mathbf{f}_i dV \quad (8-103)$$

From the divergence theorem the volume integral of the gradient of the Maxwell stress tensor in Equation (8-102) can be converted to a surface integral:

$$\int \frac{\partial T_{ij}}{\partial x_j} dV = \int \nabla \cdot \mathbf{T}_i dV = \oint \mathbf{T}_i \cdot d\mathbf{S} = \oint T_{ij} dS_j \quad (8-104)$$

Here we applied the usual divergence theorem by thinking of T_{ij} as three separate vectors \mathbf{T}_i having components $(\mathbf{T}_i)_j = T_{ij}$. The volume integral of Equation (8-102) now becomes

Momentum Conservation	$\frac{d}{dt}(\mathbf{P}_{\text{charges}} + \mathbf{P}_{\text{field}})_i = \oint T_{ij} dS_j$
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$$(8-105)$$

The capitalized momenta are the volume-integrated momentum densities. We see that the total rate of change of momentum has been expressed as a stress force acting over the bounding surface.

$$\nabla \times H = J + \partial_t D$$

$$J = \nabla \times \frac{1}{\mu_0} B - \partial_t \sum E$$

$$\nabla \times E = -\partial_t B$$

$$[(\nabla \times E) \times E]_i = \epsilon_{jkl} \partial_i E_k E_{lj} \epsilon_{jk}$$

$$(A \times B)_i = \epsilon_{ijk} A_j B_k$$

$$\epsilon_{jkl} \partial_k E_l$$

$$* \sum_j \epsilon_{jab} \epsilon_{jki} = \delta_{ak} \delta_{bi} - \delta_{ai} \delta_{bk}$$

\downarrow
 $\partial_k E_l \quad E_k$
 $E_a \partial_k E_l = E \cdot \nabla \bar{E}$
 $\sum_i \partial_i E_l$

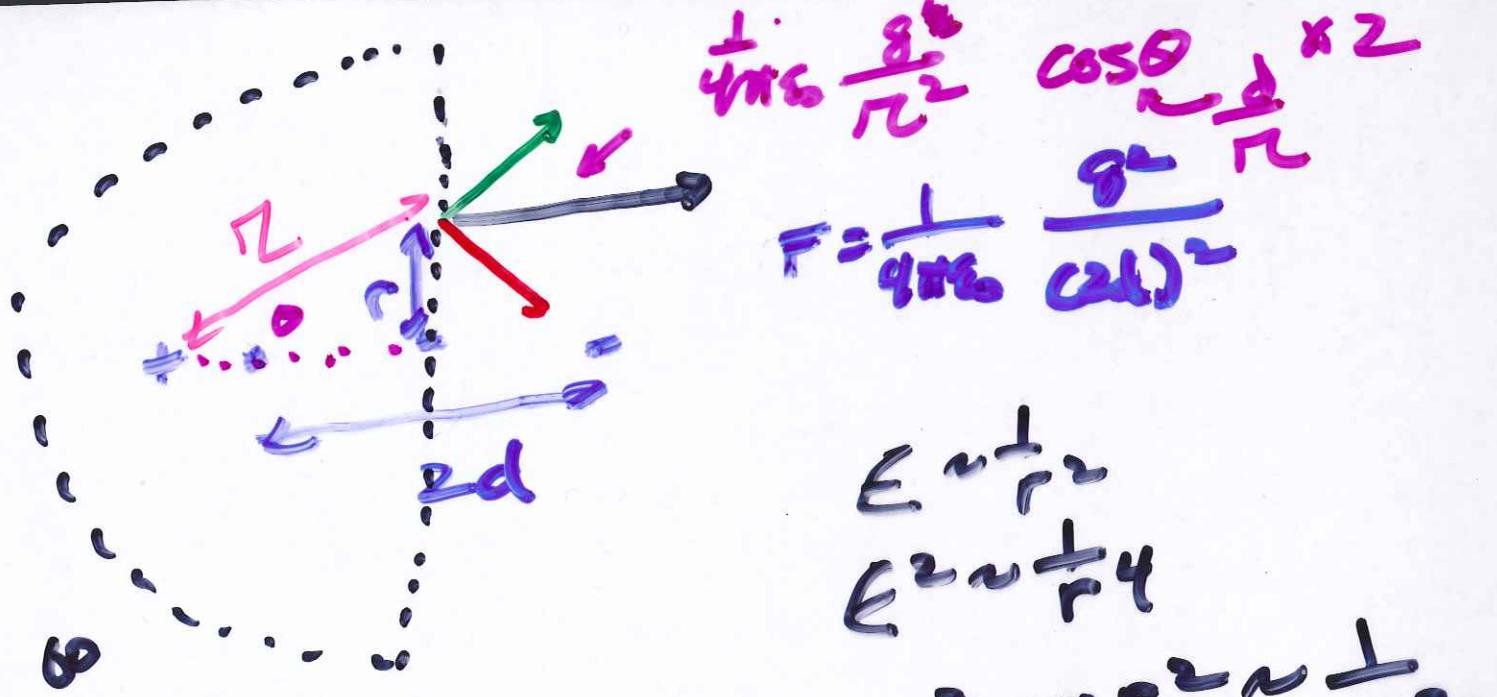
$$\sum \delta_{ai} E_l = E_a$$

$$\delta_{ij} = \begin{cases} 1 & i=j \\ 0 & i \neq j \end{cases} \quad \delta_{12} = 0 \quad \delta_{22} = 1 \quad \nabla \frac{1}{2} E^2$$

$$= E \cdot \nabla \bar{E} - \nabla \frac{1}{2} E^2$$

$$\vec{f}_T = \nabla \cdot \vec{T} - \epsilon_0 \partial_t (\vec{E} \times \vec{B})$$

$$F = \int f dV \xrightarrow{\text{d}} \int g \vec{T} \cdot \hat{n} dA$$



$$T_{ij} = \epsilon_0 \left(E_i E_j - \frac{1}{2} \delta_{ij} E^2 \right)$$

$$\begin{pmatrix} \frac{1}{2}E^2 \\ -\frac{1}{2}\delta^{12} \\ -\frac{1}{2}\delta^{21} \end{pmatrix} \begin{pmatrix} 1 \\ 0 \\ 0 \end{pmatrix}^{1/2} = \begin{pmatrix} \frac{1}{2}E^2 \\ 0 \\ 0 \end{pmatrix}$$

$$F_x = \epsilon_0 \int \frac{1}{2} E^2 dA \xrightarrow{2\pi r dr} \frac{3}{4\pi c_0} \frac{zd}{r^3}$$

$$= \epsilon_0 \int_0^\infty \frac{1}{2} \left[\frac{1}{4\pi c_0} \frac{\frac{3}{2}zd}{(r^2 + d^2)^{3/2}} \right] 2\pi r dr$$

$$= \frac{q^2 d^2}{4\pi\epsilon_0} \frac{1}{2} \int_{r_1}^0 \frac{2r dr}{(r^2 + d^2)^{3/2}} \Big|_{r_1}^{\infty}$$

$$= \frac{q^2 d^2}{4\pi\epsilon_0} \frac{1}{2} \frac{1}{2} \frac{1}{d^4}$$

$$= \frac{q^2}{4\pi\epsilon_0} \frac{1}{2} \frac{1}{d^4}$$

→ Radiation I Relativ. b

↑
arrow ↓
 $(f \uparrow \downarrow)$

Power rad q celer

$$P = \frac{1}{4\pi\epsilon_0} \frac{2}{3} \frac{8^2 a^2}{c^3} R \frac{q^2 E}{m}$$



$N R$

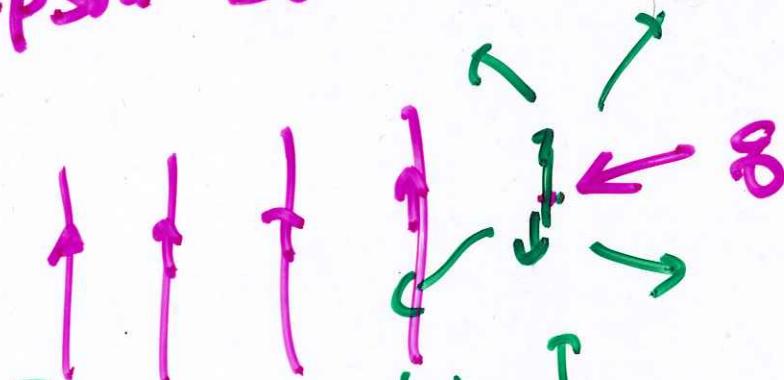


q_0

$$\frac{q^2}{4\pi\epsilon_0 R} = mc^2$$

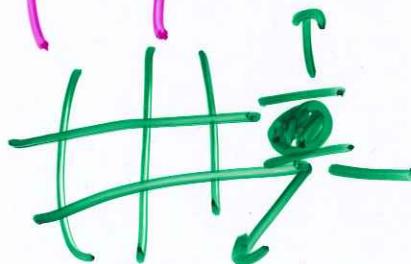
Thompson Sc. Haupts

$\approx 10^{-15} \text{ m}$
nude



$$S = \frac{1}{\mu_0 c} \frac{1}{\epsilon^2}$$

W/m^2



$$\frac{h}{mc}$$

$$d \approx \frac{1}{137}$$

$$\frac{w}{w/m^2} = 0$$

$$= \frac{8\pi}{3} R_c^2 \frac{1}{7}$$

$$\frac{8\pi}{3} \omega^2 R_c^2$$