

14-16. Letting $p_a = p_b$, we find $\rho_c g(H + T + D) + \rho_m(y - D) = \rho_c g(T) + \rho_m(y)$ and obtain

$$D = \frac{(H)\rho_c}{\rho_m - \rho_c} = \frac{(6.0 \text{ km})(2.9 \text{ g/cm}^3)}{3.3 \text{ g/cm}^3 - 2.9 \text{ g/cm}^3} = 43.5 \text{ km} .$$

14-18. (a) The force on face A of area A_A is

$$\begin{aligned} F_A &= p_A A_A = \rho_w g h_A A_A = 2\rho_w g d^3 \\ &= 2 \left(1.0 \times 10^3 \text{ kg/m}^3\right) (9.8 \text{ m/s}^2) (5.0 \text{ m})^3 = 2.45 \times 10^6 \text{ N} . \end{aligned}$$

(b) The force on face B is

$$\begin{aligned} F_B &= \int_{2d}^{3d} p dA = \int_{2d}^{3d} \rho_w g z \times d dz = \rho_w g d \left[\frac{1}{2} z^2 \right]_{2d}^{3d} = \frac{1}{2} \rho_w g d (9d^2 - 4d^2) \\ &= \frac{5}{2} \left(1.0 \times 10^3 \text{ kg/m}^3\right) (9.8 \text{ m/s}^2) (5.0 \text{ m})^3 = 3.06 \times 10^6 \text{ N} . \end{aligned}$$

Note that these figures are due to the “gauge” pressure only. If you add the contribution from the atmospheric pressure, then you need to add $F' = (1.0 \times 10^5 \text{ Pa})(5.0 \text{ m})^2 = 2.5 \times 10^6 \text{ N}$ to each of the figures above. The results would then be $5.0 \times 10^6 \text{ N}$ and $5.6 \times 10^6 \text{ N}$, respectively.

14-29. Since the object is in equilibrium:

$$\text{Buoyant Force} = \text{weight of displaced fluid} = \text{weight of object}$$

Let: ρ_w be the density of water, ρ_o be the density of oil, and ρ be the density of the object:

$$\frac{2}{3} V \rho_w g = V \rho g$$

So $\rho = \frac{2}{3} \rho_w = 667 \text{ kg/m}^3$, and

$$0.9 V \rho_o g = V \rho g = V \frac{2}{3} \rho_w g$$

So $\rho_o = \frac{2}{0.9 \cdot 3} \rho_w = 741 \text{ kg/m}^3$

14-53. (a) The friction force is

$$\begin{aligned} f &= A \Delta p = \rho_w g h A \\ &= (1.0 \times 10^3 \text{ kg/m}^3) (9.8 \text{ m/s}^2) (6.0 \text{ m}) \left(\frac{\pi}{4}\right) (0.040 \text{ m})^2 = 73.9 \text{ N} . \end{aligned}$$

Note: I have seemingly neglected the slight variation in pressure on different parts of the plug; however in fact the extra pressure at a point slightly below the center of the plug will be compensated by the lower pressure at a point symmetrically above the center of the plug.

(b) The speed of water flowing out of the hole is $v = \sqrt{2gh}$. Thus, the volume of water flowing out of the pipe in $t = 3.0 \text{ h}$ is

$$\begin{aligned} V &= A v t = \frac{\pi d^2 v t}{4} \\ &= \frac{\pi}{4} (0.040 \text{ m})^2 \sqrt{2(9.8 \text{ m/s}^2)(6.0 \text{ m})} (3.0 \text{ h})(3600 \text{ s/h}) \\ &= 147 \text{ m}^3 . \end{aligned}$$

14-59. (a) Using the notation in the problem in the equation of continuity yields:

$$AV = av$$

and in Bernoulli's equation we have:

$$P_1 + \frac{1}{2} \rho V^2 = P_2 + \frac{1}{2} \rho v^2$$

SO:

$$\begin{aligned}\Delta P = P_1 - P_2 &= \frac{1}{2} \rho (v^2 - V^2) \\ &= \frac{1}{2} \rho ((AV/a)^2 - V^2) \\ &= \frac{1}{2} \rho ((A/a)^2 - 1) V^2\end{aligned}$$

Isolating V yields:

$$\begin{aligned}\frac{2\Delta P}{\rho((A/a)^2 - 1)} &= V^2 \\ \text{or} \\ \sqrt{\frac{2\Delta P}{\rho((A/a)^2 - 1)}} &= V\end{aligned}$$

(b)

$$\begin{aligned}V &= \sqrt{\frac{2 \cdot 14 \times 10^3 \text{ Pa}}{1000 \text{ kg/m}^3 ((2)^2 - 1)}} \\ &= \sqrt{\frac{2 \cdot 14 \text{ N/m}^2}{3 \text{ kg/m}^3}} \\ &= 3.06 \text{ m/s}\end{aligned}$$

- 14-61. (a) Bernoulli's equation gives $p_A = p_B + \frac{1}{2}\rho_{\text{air}}v^2$. But $\Delta p = p_A - p_B = \rho gh$ in order to balance the pressure in the two arms of the U-tube. Thus $\rho gh = \frac{1}{2}\rho_{\text{air}}v^2$, or

$$v = \sqrt{\frac{2\rho gh}{\rho_{\text{air}}}}.$$

Note: we are neglecting here the weight of the air, i.e., a term $\rho_{\text{air}}gy$ in Bernoulli's equation and also treating air as an incompressible fluid. Is is OK since $\rho_{\text{air}} \ll \rho_{\text{alcohol}}$ and the speeds are much less than the speed of sound.

(b) The plane's speed relative to the air is

$$v = \sqrt{\frac{2\rho gh}{\rho_{\text{air}}}} = \sqrt{\frac{2(810 \text{ kg/m}^3)(9.8 \text{ m/s}^2)(0.260 \text{ m})}{1.03 \text{ kg/m}^3}} = 63.3 \text{ m/s}.$$